

Cu Ni30 Mn1 Fe

Common names: 70/30 Copper-Nickel-Iron
70/30 Cupro-nickel
Cupro-nickel, 70/30

A copper-nickel alloy with an alpha phase structure. Small amounts of iron and manganese are added to improve corrosion resistance in high-velocity (from 1.5 to about 4.5 m/s) waters, including polluted seawater. The alloy is almost insensitive to stress corrosion. It retains its strength well at moderately elevated temperatures, has good cold- and hot-working properties and is readily weldable. The most commonly used wrought forms are plate, sheet, rod and tube.

COMPOSITION (weight %)

Ni	29.0-32.0
Mn	0.5- 1.5
Fe	0.4- 1.0
Cu	rem.

1 SOME TYPICAL USES**Chemical & Marine***

Tubes and tubeplates for heavy-duty condensers, feedwater heaters and evaporators, including desalination plant.

Mechanical

Fasteners.

*Several varieties of this alloy, with higher iron and manganese contents, are used in tube form under severe conditions of impingement and erosion.

2 PHYSICAL PROPERTIES

		Metric Units	English Units
2.1	Density at 20 °C 68 °F	8.95 g/cm ³	0.325 lb/in ³
2.2	Melting range (a)	1 170-1 240 °C	2 140-2 265 °F
2.3	Coefficient of thermal expansion (linear) at: -183 to 10 °C -297 to 50 °F 20 to 300 °C 68 to 572 °F	0.000 012 per °C	0.000 007 per °F
		0.000 016 " "	0.000 009 " "
2.4	Specific heat (thermal capacity) at: 20 °C 68 °F	0.09 cal/g °C	0.09 Btu/lb °F
2.5	Thermal conductivity at: 20 °C 68 °F	0.07 cal cm/cm ² s °C	17 Btu ft/ft ² h °F
2.6	Electrical conductivity (volume) at: -269 °C -452 °F (annealed) 20 °C 68 °F (annealed or cold worked) 200 °C 392 °F (" " " ")	3 m/ohm mm ²	5% IACS
		3 " "	5 " "
		3 " "	5 " "
2.7	Electrical resistivity (volume) at: -269 °C -452 °F (annealed) 20 °C 68 °F (annealed or cold worked) 200 °C 392 °F (" " " ")	0.34 ohm mm ² /m	207 ohms (circ mil/ft)
		34 microhm cm	14 microhm in
		0.34 ohm mm ² /m	207 ohms (circ mil/ft)
		34 microhm cm	14 microhm in
2.8	Temperature coefficient of electrical resistance at: 20 °C 68 °F (annealed or cold worked) applicable over range from 0 to 100 °C 32 to 212 °F	0.000 05 per °C (5% IACS)	0.000 03 per °F (5% IACS)
2.9	Modulus of elasticity (tension) at 20 °C 68 °F annealed cold worked (b)	15 500 kg/mm ²	22 000 000 lb/in ²
		14 600 kg/mm ²	20 800 000 lb/in ²
2.10	Modulus of rigidity (torsion) at 20 °C 68 °F annealed cold worked (b)	5 750 kg/mm ²	8 200 000 lb/in ²
		5 400 kg/mm ²	7 700 000 lb/in ²

(a) The melting range covers the highest liquidus and lowest solidus temperatures over the composition range quoted. The values are based on: Hansen, M. and Anderko, K. Constitution of Binary Alloys. 2nd ed. (1958) McGraw-Hill, London, New York; more recent work (Feest, E.A. and Doherty, R.D. The Cu-Ni Equilibrium Phase Diagram. J. Inst. Metals, Vol. 99 (1971), pp. 102-103) indicates that the solidus temperature may be slightly higher.

(b) Approximately 50% cold work.

N.B.: The values shown in Section 2, which have been appropriately rounded in view of the composition range involved, are based on selected literature references.

INDEX NUMBERS RELATE TO LITERATURE REFERENCES (see page 10); INDEX LETTERS RELATE TO FOOTNOTES AT END OF TABLE

Prepared by
CONSEIL INTERNATIONAL POUR LE
DEVELOPPEMENT DU CUIVRE (CIDEC)
100, rue du Rhône - 1204 GENEVE

Distributed by
C.I.C.L.A.
Centre d'Information Du Cuivre, Laitons, Alliages
67, Boulevard Berthier, 75 Paris XVIIe

DATA SHEET No. K6
© Cu Ni30 Mn1 Fe
1972 Edition

3 FABRICATION PROPERTIES

The information given in this table is for general guidance only, since many factors influence fabrication techniques. The values shown are approximate only, since those used in practice are dependent upon form and size of metal, equipment available, techniques adopted and properties required in the material.

	Metric Units	English Units
3.1 Casting temperature range	1 325–1 400 °C	2 415–2 550 °F
3.2 Annealing temperature range	650– 850 °C	1 200–1 560 °F
Stress relieving temperature range	300– 400 °C	570– 750 °F
3.3 Hot working temperature range	925–1 025 °C	1 695–1 875 °F
3.4 Hot formability		Good
3.5 Cold formability		Good
3.6 Cold reduction between anneals		50% max.
3.7 Machinability:		See General Data Sheet No. 2
Machinability rating (free cutting brass = 100)		20
3.8 Joining methods:		See General Data Sheet No. 3.9
Soldering		Excellent
Brazing		Excellent
Oxy-acetylene welding		Good
Carbon-arc welding		Not recommended
Gas-shielded arc welding		Excellent
Coated metal-arc welding		Good
Resistance welding: spot and seam		Good
butt		Good

4 NATIONAL SPECIFICATIONS FOR MANUFACTURED FORMS

and ISO Recommendation

Country	Designation of Standards	Designation of Material in Standards	Specification for Chemical Composition ^(a)	Plate Sheet Strip	Rod	Wire	Tube	Sections	Forgings
								Shapes	
Australia . . .	SAA	—	—	—	—	—	—	—	—
Belgium . . .	NBN	—	—	—	—	—	—	—	—
Canada . . .	CSA	HC.NF301	—	HC.4.6	—	—	HC.7.3 HC.7.4	—	—
Chile	NCh (INDITECNOR)	Cu Ni30 Mn1 Fe	NCh 250. of 68	—	—	—	—	—	—
France . . .	NF	Cu Ni30 Mn1 Fe	—	—	—	—	A51-102	—	—
Germany . . .	DIN	Cu Ni30 Fe	17 664	17 670	17 672	17 672	1785 17 671	—	—
India . . .	IS	—	—	—	—	—	—	—	—
Italy . . .	UNI	Pt-Cu Ni30 Mn 1Fe	—	—	—	—	6785	—	—
Japan . . .	JIS	CNP 3 CNTF 3 CNTF 3 S	—	H 3251	—	—	H 3635	—	—
Netherlands . .	N or NEN ^(b)	—	—	—	—	—	—	—	—
South Africa . .	SABS	—	—	—	—	—	—	—	—
Spain . . .	UNE	—	—	—	—	—	—	—	—
Sweden . . .	SIS	—	—	—	—	—	—	—	—
Switzerland . .	VSM	Cu Ni30 Fe Mn	—	10 803	—	—	10 803 11 557	—	—
United Kingdom . .	BS	CN107	—	1541 2870 ^(d) 2875	—	—	378 1464 2579 (Part1) 2871	—	—
United States ^(c) . . .	ASTM	No. 715	—	B 122 B 151 B 171 B 402	B 151	—	B 111 B 359 B 395 B 466 B 467 B 543	—	—
International Organization for Standardization	ISO	Cu Ni30 Mn1 Fe	R 429	—	—	—	—	—	—

(a) Applicable when the chemical composition is not given in the specifications for wrought forms.

(b) Older specifications bear prefix N; for new specifications the NEN prefix is used.

(c) In the United States, bar is covered under the Plate-Sheet-Strip column.

(d) In metricated revision (1968); not in imperial units edition (1962).

5 MECHANICAL PROPERTIES

5.1 Mechanical properties at room temperature

Tensile properties	see tables 5.1.1/2/3
Hardness	„ „ 5.1.1/2/3
Shear Strength	„ „ 5.1.1/2/3
Modulus of elasticity (tension)	see 2.9
Modulus of rigidity (torsion)	„ 2.10

5.2 Mechanical properties at low temperature

Tensile properties	see table 5.2.1
Impact properties	„ „ 5.2.1

5.3 Mechanical properties at elevated temperature

Short-time tensile properties	see table 5.3.1
Creep properties	see tables 5.3.2.1/2/3

5.4 Fatigue properties

Fatigue strength at room temperature	see table 5.4.1
--------------------------------------	-----------------

5.1 MECHANICAL PROPERTIES AT ROOM TEMPERATURE ^(*)

5.1.1 Typical Tensile Properties and Hardness Values—Metric Units

This table is representative of practice in many European countries. For British and American practices, see tables 5.1.2 and 5.1.3, respectively.

The values shown represent reasonable approximations for general engineering use, taking account of variations in composition and manufacturing procedures. For design purposes, national specifications should be consulted.

For a given temper, individual elongation values may show some variation above or below the typical values indicated.

Form	Temper	Tensile Strength kg/mm ²	Proof Stress 0.2% offset kg/mm ²	Elongation		Hardness		Shear Strength kg/mm ²	Typical Size Related to Properties Shown ^(a)
				%	gauge length	Brinell	Vickers		
Plate Sheet Strip	Annealed	36	15	42	5.65√S ₀	85	89	27	1–20 mm thick
	Hot Rolled	38	16	38	5.65√S ₀	90	95	28	10–50 mm thick
	Typical Cold Worked Temper	50	43	16	5.65√S ₀	140	145	35	1–5 mm thick
Rod ^(c)	Annealed	40	17	40	5.65√S ₀	95	100	30	6–40 mm diam. or equivalent area
	Typical Cold Worked Temper	50	42	18	5.65√S ₀	130	135	35	6–25 mm diam. or equivalent area
Tube ^(b)	Annealed (grain size 0.025 mm)	42	17	42	5.65√S ₀	90	95	31	10–30 mm O.D. 1–3 mm wall
	Typical Cold Drawn Temper	52	45	18	5.65√S ₀	145	150	36	10–30 mm O.D. 1–2 mm wall

(a) It is possible to obtain sizes outside the ranges given in this column, but information on their mechanical properties should be obtained from the metal manufacturers.

(b) Tubes for condensers and heat exchangers are generally supplied in the annealed temper whose representative mechanical properties are shown.

(c) The mechanical properties will be largely dependent upon the size and cross-sectional area or complexity of the product.

5.1.2 Typical Tensile Properties and Hardness Values—SI and English Units

This table is based on British practice. For other European and American practices, see tables 5.1.1 and 5.1.3, respectively.

The values shown represent reasonable approximations for general engineering use, taking account of variations in composition and manufacturing procedures. For design purposes, national specifications should be consulted.

For a given temper, individual elongation values may show some variation above or below the typical values indicated.

Form	Temper ^(a)	Tensile Strength		Proof Stress 0.1% offset		Elongation		Vickers Hardness	Shear Strength		Typical Size Related to Properties Shown ^(b)
		hbar	ton/in ²	hbar	ton/in ²	%	gauge length		hbar	ton/in ²	
Plate	Annealed	39	25	15	10	42	5.65√S ₀	95	29	19	—
	Hot Rolled As-Manufactured	40	26	17	11	40	5.65√S ₀	105	31	20	12–50 mm (0.5–2 in.) thick
Sheet Strip	Annealed	39	25	15	10	45	50 mm (2 in.)	95	29	19	—
	Hot Rolled As-Manufactured	43	28	20	13	40	50 mm (2 in.)	120	32	21	3–10 mm (0.125–0.375 in.) thick
Tube ^(c)	Annealed (grain size 0.025 mm)	42	27	17	11	42	5.65√S ₀	105	31	20	—
	Cold Drawn or Temper Annealed As-Drawn (hard)	51	33	37	24	25	5.65√S ₀	150	32	21	50–255 mm (2–10 in.) O.D. 2–5 mm (0.08–0.2 in.) wall
	Temper Annealed	43	28	20	13	40	5.65√S ₀	120	32	21	
	Temper Annealed	49	32	34	22	30	5.65√S ₀	140	37	24	6–50 mm (0.25–2 in.) O.D.
	As-Drawn As-Drawn (hard)	56 66	36 43	46 57	30 37	15 7	5.65√S ₀ 5.65√S ₀	170 190	39 37	25 24	0.5–2 mm (0.02–0.08 in.) wall

(a) The recognised temper designations used in the relevant British Standards are also given.

(b) It is possible to obtain sizes outside the ranges given in this column, but information on their mechanical properties should be obtained from the metal manufacturers.

(c) Intermediate tube tempers are generally obtained by temper annealing. Drawn tubes are usually stress relieved after the final draw. Tubes for condensers and heat exchangers are mainly supplied in the tempers whose representative mechanical properties are printed in **bold type**.

(*) It will be noted that tables 5.1.1, 5.1.2 and 5.1.3, giving typical tensile properties and hardness values in Metric, SI and English, and American units respectively are not directly comparable. This is because the properties quoted reflect to some extent the metalworking techniques, specification practices, and testing procedures in the countries concerned, and in view of the different sizes of products referred to in these tables. Individual manufacturers of semi-fabricated products, can, however, normally meet the requirements of any national standard.

5.1.3 Typical Tensile Properties and Hardness Values—American Units

This table is based on American practice and the temper designations shown are those referred to in ASTM and other American Standards. For British and other European countries' practices, see tables 5.1.2 and 5.1.1, respectively.

The values shown represent reasonable approximations for general engineering use, taking account of variations in composition and manufacturing procedures. For design purposes, national specifications should be consulted.

For a given temper, individual elongation values may show some variation above or below the typical values indicated.

Form	Temper	Tensile Strength psi	Yield Strength 0.5% extension under load psi	Elongation		Rockwell Hardness			Shear Strength psi	Typical Size Related to Properties Shown ^(a)
				%	gauge length	F	B	30 T		
Flat Products (Plate, Sheet, Strip)	As Hot Rolled	55 000	20 000	45	2 in.	—	35	—	41 000	1.0 in. thick
		50 000	20 000	35	2 in.	—	—	—	37 000	2.0 in. thick
	Annealed	55 000	18 000	36	2 in.	—	40	—	41 000	0.040 in. thick
		54 000	22 000	40	2 in.	—	35	—	40 000	1.0 in. thick
		Cold Worked	73 000	67 000	4	2 in.	—	80	—	51 000
Half Hard	81 500	76 000	3	2 in.	—	85	—	52 000	"	
Hard	86 000	79 000	3	2 in.	—	87	—	52 000	"	
Extra Hard	89 000	80 000	3	2 in.	—	88	—	48 000	"	
Rod ^(b)	Annealed	55 000	20 000	45	2 in.	—	37	—	41 000	1.0 in. diam.
	Cold Worked	75 000	70 000	15	2 in.	—	80	—	52 000	1.0 in. diam.
		Half Hard	85 000	78 000	15	2 in.	—	81	—	55 000
Tube ^(c)	Annealed (grain size 0.025 mm)	60 000	25 000	45	2 in.	80	45	—	45 000	1.0 in. O.D. × 0.065 in. wall
		54 000	—	45	2 in.	77	36	—	40 000	4.5 in. O.D. × 0.109 in. wall
	Cold Worked	75 000	68 000	15	2 in.	—	80	—	52 000	1.0 in. O.D. × 0.065 in. wall
		Light Drawn	84 000	—	4	2 in.	—	—	—	55 000
Hard Drawn	84 000	—	4	2 in.	—	—	—	55 000	0.75 in. O.D. × 0.049 in. wall	

(a) It is possible to obtain sizes different from those given in this column, but information on their mechanical properties should be obtained from the metal manufacturers.

(b) The mechanical properties will be largely dependent upon the size and cross-sectional area or complexity of the product.

(c) Tubes for condensers and heat exchangers are generally supplied in annealed or drawn and stress-relieved tempers.

5.2 MECHANICAL PROPERTIES AT LOW TEMPERATURE

5.2.1 Tensile Properties—Impact Properties

Form	Temper	Testing Temperature		Tensile Strength			Proof Stress		Elongation		Reduction of Area %	Impact Strength	
		°C	°F	kg/mm ²	ton/in ²	psi	0.2% offset kg/mm ²	Yield Strength 0.5% ext. under load psi	%	gauge length		kg m/cm ²	ft lb
Rod ⁽¹⁾ 12 mm diam. 0.47 in. diam.	Cold Worked	20	68	65	41.5	92 500	—	56 900 ^(a)	12	16 mm	—	—	—
		0	32	65	41.5	92 500	—	61 200 ^(a)	13	16 mm	—	—	—
		-100	-148	70	44.5	99 500	—	76 800 ^(a)	17	16 mm	—	—	—
		-196	-321	80	51	114 000	—	99 600 ^(a)	24	16 mm	—	—	—
		-224	-371	83	52.5	118 000	—	107 000 ^(a)	22	16 mm	—	—	—
		-247	-413	90	57	128 000	—	114 000 ^(a)	20	16 mm	—	—	—
		-269	-452	95	60.5	135 000	—	121 000 ^(a)	18	16 mm	—	—	—
Rod ^{(d) (2)} 19 mm diam. 0.75 in. diam.	Annealed	22	72	40.5	26	57 800	—	18 700	47	4.52√S ₀	68	19.9 ^(b)	115 ^(b)
		-78	-108	48	30.5	68 000	—	22 200	48	4.52√S ₀	70	19.7 ^(b)	114 ^(b)
		-197	-323	63	40	89 800	—	31 600	52	4.52√S ₀	70	19.7 ^(b)	114 ^(b)
		-253	-423	72.5	46	103 100	—	38 100	51	4.52√S ₀	66	19.7 ^(b)	114 ^(b)
		-269	-452	73.5	46.5	104 600	—	40 100	48	4.52√S ₀	65	—	—
Rod ^{(3) (4)} 22 mm diam. 0.875 in. diam.	Annealed	24	75	38	24.5	54 400	15.1 ^(c)	—	52	2 in.	80.5	—	—
		-30	-22	41	26	58 600	15.5 ^(c)	—	49.5	2 in.	79	—	—
		-78	-108	45	28.5	64 300	16.9 ^(c)	—	56	2 in.	77.5	—	—
		-140	-220	50.5	32	71 900	19.3 ^(c)	—	57.5	2 in.	77.5	—	—
		-196	-320	59	37.5	83 700	21.7 ^(c)	—	61.5	2 in.	77.5	—	—

(a) This value was originally reported in kg/mm²; in this table it is given in psi to 3 significant figures.

(b) Charpy test; 10 × 10 × 55 mm specimen; 45° V notch 2 mm deep; cross-sectional area at the notch 0.8 cm².

(c) This value was originally reported in psi; in this table it is given in kg/mm² to 3 significant figures.

(d) Tensile specimen 6.35 mm (0.25 in.) diam.

N.B.: — Original values are printed in **bold type**; other values are converted.

— All converted values for impact strength are to be taken as indicative only; the impact energy has been converted from ft lb into kg m/cm² taking into account the actual cross-sectional area of the specimen at the notch.

— Data not available: Proof stress, 0.1% offset.

5.3 MECHANICAL PROPERTIES AT ELEVATED TEMPERATURE
5.3.1 Short-Time Tensile Properties

Form	Temper	Testing Temperature		Tensile Strength			Proof Stress			Elongation	
		°C	°F	kg/mm ²	ton/in ²	psi	0.2% offset kg/mm ²	0.1% offset ton/in ²	Yield Strength 0.5% ext. under load psi	%	gauge length
Plate ⁽⁵⁾	Hot Rolled	20	68	37.5	23.9	53 500	12.4 ^(a)	7.4	—	50	2 in.
		66	150	35.5	22.7	51 000	12.4 ^(a)	7.5	—	49	2 in.
		121	250	33.5	21.4	48 000	11.5 ^(a)	6.7	—	48	2 in.
		177	350	32.5	20.5	46 000	10.4 ^(a)	6.3	—	48	2 in.
		232	450	31	19.7	44 000	10.6 ^(a)	6.2	—	46	2 in.
		288	550	30	19.0	42 500	10.2 ^(a)	6.0	—	55	2 in.
		343	650	29	18.5	41 500	9.29 ^(a)	5.2	—	54	2 in.
		371	700	29	18.3	41 000	9.45 ^(a)	5.6	—	63	2 in.
Plate ⁽⁶⁾	Hot Worked	20	68	38	24	54 000	13.5	—	—	—	—
		100	212	38	24	54 000	13.5	—	—	—	—
		200	392	35.5	22.5	50 500	12	—	—	—	—
		300	572	33	21	47 000	11.5	—	—	—	—
		400	752	30	19	42 500	10	—	—	—	—
Strip ⁽⁷⁾ 2 mm 0.08 in.	Annealed	20	68	40.5	25.8	58 000	—	7.9	—	44	2 in.
		100	212	37.5	23.8	53 500	—	7.5	—	40	2 in.
		200	392	34.5	21.9	49 000	—	6.6	—	37	2 in.
		300	572	32.5	20.5	46 000	—	6.1	—	34	2 in.
		400	752	30.5	19.4	43 500	—	5.8	—	31	2 in.
		500	932	26	16.4	36 500	—	5.4	—	20	2 in.
Rod ⁽⁸⁾ 14 mm diam. 0.55 in. diam.	Annealed	20	68	44	28	62 500	16	—	—	38	11.3√S ₀
		100	212	41	26	58 500	11	—	—	36	11.3√S ₀
		200	392	38	24	54 000	11	—	—	33	11.3√S ₀
		300	572	35	22	50 000	11	—	—	32	11.3√S ₀
		390	734	33.5	21.5	47 500	11	—	—	29	11.3√S ₀
		500	932	28	18	40 000	11	—	—	22	11.3√S ₀
		600	1 112	19	12	27 000	9	—	—	16	11.3√S ₀
		700	1 292	11	7	15 500	8	—	—	6	11.3√S ₀
Rod ⁽⁹⁾ 22 mm diam. 0.875 in. diam.	Cold Worked 25%	24	75	52.5	33.5	74 500	50.9 ^(b)	—	—	19	2 in.
		149	300	48	30.5	68 600	45.7 ^(b)	—	—	17	2 in.
		371	700	40.5	25.5	57 600	39.0 ^(b)	—	—	13	2 in.
		482	900	30.5	19.5	43 600	27.1 ^(b)	—	—	11.5	2 in.
		649	1 200	12	7.5	16 900	6.82 ^(b)	—	—	26	2 in.
		816	1 500	5	3	7 200	2.88 ^(b)	—	—	16	2 in.
		927	1 700	3	2	4 110	1.16 ^(b)	—	—	22	2 in.
	Cold Worked 70%	24	75	67	42.5	95 200	65.0 ^(b)	—	—	16	2 in.
		149	300	61.5	39	87 500	56.8 ^(b)	—	—	16	2 in.
		371	700	51.5	33	73 600	50.0 ^(b)	—	—	11	2 in.
		482	900	40	25.5	56 900	37.0 ^(b)	—	—	14	2 in.
		649	1 200	12	7.5	16 900	6.89 ^(b)	—	—	29	2 in.
		816	1 500	5	3	6 990	2.60 ^(b)	—	—	19	2 in.
		927	1 700	2.5	1.5	3 680	1.12 ^(b)	—	—	22.5	2 in.
Rod ^{(9) (c)} 25 mm diam. 1.0 in. diam.	Annealed	28	82	45	28.5	64 100	—	—	32 000	34.5	2 in.
		260	500	37.5	24	53 300	—	—	26 300	31.5	2 in.
		343	650	34.5	22	49 200	—	—	25 000	27.0	2 in.
		427	800	33	21	46 700	—	—	22 500	25.6	2 in.
		510	950	26	16.5	37 250	—	—	21 500	16.2	2 in.
		593	1 100	18.5	12	26 550	—	—	20 000	12.3	2 in.
Rod ⁽¹⁰⁾ 27 mm diam. 1.1 in. diam.	Annealed (grain size 0.025–0.035 mm)	20	68	41.5	26.5	59 500	13.7 ^(a)	8.6	—	56	4√S ₀
		250	482	35	22.2	49 500	10.9 ^(a)	6.8	—	45	4√S ₀
		350	662	34	21.6	48 500	10.4 ^(a)	6.5	—	39	4√S ₀
		450	842	31.5	20.0	45 000	10.7 ^(a)	6.6	—	42	4√S ₀
		550	1 022	26.5	16.7	37 500	11.8 ^(a)	6.8	—	33	4√S ₀
Condenser ⁽¹¹⁾ Tube	Annealed	20	68	43	27.5	61 000	16	—	—	38	11.3√S ₀
		100	212	39	25	55 500	14.5	—	—	35	11.3√S ₀
		200	392	36	23	51 000	13.5	—	—	36	11.3√S ₀
		300	572	34.5	22	49 000	12.0	—	—	28	11.3√S ₀
		400	752	33	21	47 000	11.0	—	—	30	11.3√S ₀
		500	932	24	15	34 000	10	—	—	25	11.3√S ₀
		600	1 112	17	11	24 000	8	—	—	25	11.3√S ₀

(a) This value was originally reported in ton/in²; in this table it is given in kg/mm² to 3 significant figures.

(b) This value was originally reported in psi; in this table it is given in kg/mm² to 3 significant figures.

(c) Alloy containing 0.40% Mn.

N.B.: — Original values are printed in **bold type**; other values are converted.

— Further data can be obtained from the following papers:

■ Simmons, W.F., Sirois, B.J., Williams, D.N. & Jaffee, R.I. Properties of 70–30 Copper-Nickel Alloy at Temperatures Ranging up to 1 050°F. Proc. ASTM, Vol. 59 (1959), pp. 1035–1051. (data for cold drawn and stress relieved rod; alloy containing 0.35% Mn).

■ Reference ⁽³⁾.

5.3.2 Creep Properties
5.3.2.1 Original Creep Data

Form	Temper	Testing Temperature		Stress			Duration h	Total Extension % ^(a)	Intercept %	Minimum Creep Rate % per 1 000 h
		°C	°F	kg/mm ²	ton/in ²	psi				
Rod ⁽¹²⁾ (b) 3 mm diam. 0.125 in. diam.	Annealed (grain size 0.020 mm)	149	300	3.2	2.0	4 550	2 600	0.033	0.010	< 0.000 1
				10.6	6.7	15 100	2 600	0.109	0.022	< 0.000 1
				14.0	8.9	19 900	4 400	0.884	0.022	0.000 4
				20.0	12.7	28 450	5 200	3.230	0.025	0.001 0
				23.0	14.6	32 700	3 700	4.532	0.030	0.000 6
		11.2	7.1	15 950	4 100	0.167	0.006	< 0.000 2		
	Cold Worked 84%	260	500	3.5	2.2	4 980	2 780	0.031	0.001	< 0.000 1
				7.2	4.6	10 250	5 000	0.075	0.012	< 0.000 5
				11.0	7.0	15 650	5 000	0.310	0.015	0.000 9
		14.9	9.4	21 150	5 000	1.498	0.030	0.003 7		
		18.6	11.8	26 500	5 100	2.775	0.028	0.005 3		
		21.5	13.7	30 650	5 100	4.671	0.048	0.008 4		
Cold Worked 84%	149	300	14.0	8.9	19 900	3 600	0.108	0.018	< 0.000 1	
			24.5	15.6	34 900	3 700	0.174	0.016	< 0.000 1	
			34.9	22.1	49 600	5 150	0.259	0.024	0.000 5	
	42.1	26.8	59 950	4 650	0.345	0.036	0.000 9			
	260	500	3.5	2.2	4 960	2 760	0.036	0.012	0.000 7	
			7.1	4.5	10 100	4 980	0.074	0.024	0.001 1	
14.6			9.3	20 800	4 800	0.124	0.023	0.001 6		
28.7	18.2	40 800	4 800	0.243	0.049	0.002 4				
34.6	21.9	49 150	5 100	0.322	0.066	0.003 0				
42.1	26.7	59 850	5 750	0.648	0.267	0.012				
Rod ⁽¹³⁾ 19 mm diam. 0.75 in. diam.	Cold Worked and Stress relieved	316	600	28.1	17.8	40 000	500	0.255 ^(c)	—	0.015 ^(d)
				35.1	22.3	50 000	500	0.426	—	0.02 ^(d)
				38.6	24.5	55 000	500	0.940	—	0.08 ^(d)
		399	750	12.6	8.0	18 000	2 500	0.219	—	0.015
				17.6	11.1	25 000	2 500	0.319 ^(c)	—	0.032
				21.1	13.4	30 000	1 500	0.359 ^(c)	—	0.055
	24.6			15.6	35 000	1 000	0.490 ^(c)	—	0.17	
	28.1			17.8	40 000	1 000	0.818	—	0.40	
	31.6	20.1	45 000	1 500	3.25	—	1.0			
	454	850	4.9	3.1	7 000	2 500	0.142	—	0.019	
			9.8	6.2	14 000	1 500	0.339	—	0.072	
			17.6	11.1	25 000	1 000	0.993	—	0.61	
	21.1	13.4	30 000	1 500	9.80	—	2.2			
	510	950	1.4	0.89	2 000	1 500	0.096	—	0.032	
			4.2	2.7	6 000	1 000	0.292	—	0.18	
	12.6	8.0	18 000	1 500	11.2	—	3.4			
	566	1 050	1.0	0.67	1 500	500	0.185	—	0.3	
			7.3	4.4	10 000	500	7.20	—	7	
Rod ⁽¹⁴⁾ (e)	Annealed	149	300	30	19	42 670	2 370	13.16	13.16	0 ^(f)
				32.3	20.5	46 000	2 182	19.84	19.84	0 ^(f)
33	21			47 000	2 340	20.42	20.42	0 ^(f)		
482	900	13	8.3	18 670	2 752	49.0	2.3	9.5 ^(f)		
Rod ⁽¹⁵⁾ (e)	Cold Worked 40%	371	700	30	19	42 670	8 490	3	0.27	0.33 ^(f)
		482	900	11.2	7.1	16 000	14 044	46	0.32	0.39 ^(f)
				15	9.5	21 330	4 190	23	0.45	1.5 ^(f)
649	1 200	1	0.64	1 450	5 002	28.5	0.40	2.65 ^(f)		

(a) Total Extension = Initial Extension + Total creep = Initial extension + Intercept + (Minimum Creep Rate × Duration).

(b) Fe content 0.03%.

(c) Extrapolated value.

(d) Lowest creep rate within duration of test.

(e) Creep specimen 0.505 in. diam.

(f) Average second-stage creep rate.

N.B.: — Original values are printed in **bold type**; other values are converted.
— Further data can be obtained from refs. (14) and (15).

5.3.2.2 Stress for Designated Creep Rate

Form	Temper	Testing Temperature		Stress for Designated Creep Rate											
				0.000 4% per 1 000 h			0.001% per 1 000 h			0.01% per 1 000 h			0.1% per 1 000 h		
		°C	°F	kg/mm ²	ton/in ²	psi	kg/mm ²	ton/in ²	psi	kg/mm ²	ton/in ²	psi	kg/mm ²	ton/in ²	psi
Rod ^(b) ⁽¹²⁾ 3 mm diam. 0.125 in. diam.	Annealed (grain size 0.020 mm)	149	300	—	—	—	16.9	10.7	24 000	24.6 ^(a)	15.6 ^(a)	35 000^(a)	—	—	—
		260	500	—	—	—	11.2	7.1	16 000	21.1 ^(a)	13.4 ^(a)	30 000^(a)	—	—	—
	Cold Worked 84%	260	500	—	—	—	5.6	3.6	8 000	—	—	—	—	—	—
Rod ⁽¹³⁾ 19 mm diam. 0.75 in. diam.	Cold Worked and Stress relieved	316	600	—	—	—	—	—	—	33.7	21.4	48 000	—	—	—
		371	700	—	—	—	—	—	—	18.6	11.8	26 500	—	—	—
		399	750	—	—	—	—	—	—	10.5	6.7	15 000	—	—	—
		454	850	—	—	—	—	—	—	3.5	2.2	5 000	—	—	—
		510	950	—	—	—	—	—	—	0.56	0.36	800	—	—	—
Rod ⁽¹⁰⁾ 27 mm diam. 1.1 in. diam.	Annealed (grain size 0.025–0.035 mm)	350	662	—	—	—	—	—	—	25.2	16.0	35 800	14.2	9.0	20 200
		450	842	—	—	—	—	—	—	10.2	6.5	14 600	5.7	3.6	8 100
		550	1 022	—	—	—	—	—	—	1.6	1.0	2 200	0.47 ^(a)	0.3 ^(a)	670 ^(a)
Rod ⁽¹⁶⁾	Annealed	399	750	6.3	4.0	9 000	—	—	—	—	—	—	—	—	—
	Cold Worked ^(c)	399	750	—	—	—	—	—	—	6.4	4.1	9 100	—	—	—

(a) Extrapolated value.

(b) Fe content 0.03%.

(c) Tensile strength of material at 85°F (29°C) quoted as 64 700 psi in original document but amount of cold work not defined.

N.B.: Original values printed in **bold type**; other values are converted.

5.3.2.3 Stress for Rupture

Form	Temper	Testing Temperature		Stress for Rupture			Time for Rupture h		
		°C	°F	kg/mm ²	ton/in ²	psi			
Rod ⁽¹³⁾ 19 mm diam. 0.75 in. diam.	Cold Worked and Stress relieved	399	750	31.6	20.1	45 000	2 124.4		
				35.2	22.3	50 000			
				38.7	24.6	55 000			
		454	850	21.1	13.4	30 000	1 539.7		
				24.6	15.6	35 000			
				28.1	17.9	40 000			
				31.6	20.1	45 000			
		510	950	12.7	8.0	18 000	1 839.6		
				19.0	12.1	27 000			
				24.6	15.6	35 000			
		566	1 050	7.0	4.5	10 000	968.6		
				13.4	8.5	19 000			
				16.9	10.7	24 000			
		Rod ⁽⁹⁾ 25 mm diam. 1 in. diam.	Annealed	260	500	36.9	23.4	52 500	> 3 000 ^(a)
						35.2	22.3	50 000	
				343	650	33.4	21.2	47 500	121.0
31.6	20.1					45 000			
28.1	17.9					40 000			
427	800			24.6	15.6	35 000	7.6		
				22.8	14.5	32 500			
				21.1	13.4	30 000			
				17.6	11.2	25 000			
510	950			15.8	10.0	22 500	3.3		
				14.8	9.4	21 000			
				14.1	8.9	20 000			
				12.7	8.0	18 000			
				10.5	6.7	15 000			

(a) Test stopped after 3 000 h.

N.B.: — Original values are printed in **bold type**; other values are converted.

— Further data can be obtained from the following papers:

- Bearham, J.H. and Parker, R.J. Elevated-Temperature Tensile, Stress-Rupture and Creep Data for Six Copper-Base Materials. Metallurgia (Manchr) Vol. 78, (1968), pp. 9–14.
- Blucher, J. T. and Grant, N. J. Recrystallization, Tensile and Stress-Rupture Properties of Nickel-Copper Alloys. Proc. ASTM, Vol. 62 (1962), pp. 593–601.
- Parker, R. J. Estimation of Stress-Rupture Properties from Hot Hardness Tests. Metallurgia (Manchr), Vol. 67 (1963), pp. 219–223.

5.4 FATIGUE PROPERTIES

5.4.1 Fatigue Strength at Room Temperature

Form	Temper	Number of Cycles $\times 10^6$	Metric Units kg/mm ²		English Units ton/in ²		American Units psi	
			Tensile Strength	Fatigue Strength	Tensile Strength	Fatigue Strength	Tensile Strength	Fatigue Strength
Plate ⁽¹⁷⁾	Annealed	100	~41	~14 ^(a)	~26	~ 9 ^(a)	~58 000	~20 000 ^(a)
Rod ⁽¹⁸⁾ 14 mm diam. 0.56 in. diam.	Cold Drawn 33%	100	57.5	24.5 ^(b)	36.5	15.5 ^(b)	81 700	34 500 ^(b)
Rod ⁽¹⁹⁾ 20 mm diam. 0.8 in. diam.	Cold Worked	50	55	20 ^(a)	35	12.5 ^(a)	78 500	28 500 ^(a)
Rod ⁽²⁰⁾ 25 mm diam. 1 in. diam.	Annealed	(e)	38.5	15.5	24.5	10	55 000	22 000
	Cold Drawn 50%	(e)	60	22.5	38	14.5	85 000	32 000
Tube ⁽²¹⁾ 280 mm I.D., 10 mm wall 11 in. I.D., 0.375 in. wall	Annealed	100	41	14.5 ^(c)	26.1	9.2 ^(c)	58 500	20 500 ^(c)
Tube ⁽²²⁾	Soft	100	35	15	22	9.5	50 000	21 500
	Cold Worked and Stress Relieved	100	45	18 ^(d)	28.5	11.5 ^(d)	64 000	25 500 ^(d)

(a) Rotating-cantilever test.

(b) Rotating-beam test.

(c) Direct-stress test.

(d) Bending fatigue test.

(e) Number of cycles not stated in original document.

N.B.: — Original values are printed in **bold type**; other values are converted.

— Further data can be obtained from the following papers:

- Tewes, W.A. and Gross, M.R. Investigation of the Low-Cycle Fatigue Behavior of Non-Ferrous Metals for Heat Exchangers and Salt-Water Piping. U.S. Naval EES Rept. 910 196A (1962).
- Czyryca, E.J. and Gross, M.R. Low-Cycle Fatigue of Non-Ferrous Alloys for Heat Exchangers and Salt-Water Piping. U.S. Navy MEL Rept. 26/66 (1966).
- Gross, M.R. Low-Cycle Fatigue of Materials for Submarine Construction. U.S. Naval EES Rept. 91-197D (1963); also paper 690B at SAE-ASNE National Aero-Nautical Meeting, Washington, 8-11 April, 1963.
- Gibbons, W.G. Strain-Cycle Fatigue of 70-30 Copper-Nickel. Trans. ASME, Ser. D, Vol. 88 (1966), No. 2, pp. 552-554.
- Blomfield, J.A. and Jackson, P.B.M. Fatigue Tests on Some Cupro-Nickel Pipe Bends and a Comparison of Some Failure Prediction Methods. First Int. Conf. Pressure Vessels Technology, Part 2: Materials and Fabrication. ASME (1969), pp. 1221-1231.
- Gross, M.R. and Czyryca, E.J. Correlation Between Flexural and Direct-stress Low-Cycle Fatigue Tests. Naval Ship Research and Development Center, Annapolis, Maryland, U.S.A. Rept. No. 2460 (1967) (AD 656746).
- Gross, M.R. and Schwab, R.C. Fatigue Properties of Non-Ferrous Alloys for Heat Exchangers, Pumps and Piping. U.S. Navy Marine Engng. Lab., Annapolis, Md. R and D Rept. No. 232/66 (1966) (AD 633771); also J. Engng. for Power (1967), July, pp. 345-352.

REFERENCES

MECHANICAL PROPERTIES (Section 5)

- (1) Fushimi, K., Yonemitsu, H., Okamoto, H. and Fukushima, E. Tensile Properties of Various Materials at Cryogenic Temperatures. *Advances in Cryogenic Engng.*, Vol. 15 (1970), pp. 102-108. Plenum Press, New York, London.
- (2) Reed, R.P. and Mikesell, R.P. Low-Temperature (295 to 4 K) Mechanical Properties of Selected Copper Alloys. *J. Materials*, Vol. 2 (1967), No. 2, pp. 370-392.
- (3) Jenkins, W.D., Digges, T.G. and Johnson, C.R. Tensile Properties of Copper, Nickel and 70% Copper - 30% Nickel and, 30% Copper - 70% Nickel Alloys at High Temperatures. *J. Res. Nat. Bureau Standards*, Vol. 58 (1957), pp. 201-211.
- (4) Geil, G.W. and Carwile, N.L. Tensile Properties of Copper, Nickel and Some Copper-Nickel Alloys at Low Temperatures. U.S. Dept. Commerce, Nat. Bureau of Standards, Circular 520 (1952), pp. 67-96.
- (5) Ashbolt, D. and Bowers, J.E. The Properties of Copper and Copper Alloys at Elevated Temperatures. BNFMRA Research Report A1550 (1965).
- (6) Private communication from Vereinigte Deutsche Metallwerke AG., Germany.
- (7) Benson, N.D. and Pittam, S.E., Proof Stress Values at Elevated Temperatures of 80/20 and 70/30 Copper-Nickel Alloys. Imperial Metal Industries, Ltd., England. Research Dept. Rept. MD/RR/39/49 (1949).
- (8) Private communication from Wieland-Werke, AG, Germany.
- (9) Donachie Jr., M.J., Steele, R.K. and Shephard, R.G. Elevated-Temperature Behavior of Annealed 70-30 Copper-Nickel. *Proc. ASTM*, Vol. 63 (1963), pp. 598-604.
- (10) Bearham, J.H. and Parker, R.J. Elevated - Temperature Tensile, Stress-Rupture and Creep Data for Six Copper-Base Materials. *Metallurgia (Manchr)*, Vol. 78 (1968), pp. 9-14.
- (11) Nothing, F.W. Kupfer-Nickel-Legierungen mit weniger als 50% Nickel. Nickel-Informationsbüro GmbH, Dusseldorf. Publication No. 7 (1964), 76 pp.
- (12) Upthegrove, C. and Burghoff, H.L. Elevated - Temperature Properties of Coppers and Copper-Base Alloys. American Society for Testing and Materials, Philadelphia, Pa. (1956) (ASTM Spec. Tech. Pub. No. 181).
- (13) Simmons, W.F., Sirois, B.J., Williams, D.N. and Jaffee, R.I. Properties of 70-30 Copper-Nickel Alloy at Temperatures Ranging up to 1050°F. *Proc. ASTM*, Vol. 59 (1959), pp. 1035-1051.
- (14) Jenkins, W.D. and Johnson, C.R. Creep of Annealed Nickel, Copper, and Two Nickel-Copper Alloys. *J. Res. Nat. Bureau Standards*, Vol. 60 (1958), pp. 173-191.
- (15) Jenkins, W.D. and Willard, W.A. Creep of Cold-Drawn Nickel, Copper, 70% Nickel-30% Copper, and 30% Nickel-70% Copper Alloys. *J. Res. Nat. Bureau Standards*, Vol. 66C (1962) pp. 59-76.
- (16) Copper Metals by Anaconda: Their Properties and Applications. Anaconda American Brass Co., Connecticut. Publ. B-40 (1961). p. 38.
- (17) Czyryca, E.J. and Schwab, R.C. Effect of Mean Deflection on the Low-Cycle Flexural Fatigue Behavior of Annealed 70-30 Cupro-Nickel. Naval Ship Research and Development Center, Annapolis, Md. Rept. No. 2445 (1967). (AD 656574).
- (18) Burghoff, H.L. and Blank, A.I. Fatigue Characteristics of Some Copper Alloys. *Proc. ASTM*, Vol. 47 (1947), pp. 695-712.
- (19) Weller, J. Ein Beitrag zum Schwingungs korrosionsverhalten der Nichteisenmetalle. Institut für Leichtbau, IfL - Mitteilungen, Dresden, Vol. 8(1969) pp. 349-360.
- (20) Wilkins, R.A. and Bunn, E.S. Copper and Copper-Base Alloys. McGraw - Hill Book Co., New York (1943).
- (21) Bowers, J.E., Bradley, J.N. and Griffith, E.C. Resistance of High-Strength and Zirconium - Containing Cupro-nickels to High-Strain Fatigue in Sea Water: Final Report. BNFMRA Research Report A1714 (1968).
- (22) Private communication from Kabelmetall, Osnabrück, Germany.